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(71) Applicant: **SHELL INTERNATIONALE  
RESEARCH MAATSCHAPPIJ B.V.**  
**Carel van Bylandtlaan 30**  
**NL-2596 HR Den Haag (NL)**

(72) Inventor: **Jacobs, Ludovicus Leonardus  
Gerardus**  
**Badhuisweg 3**  
**NL-1031 CM Amsterdam (NL)**  
Inventor: **Lednor, Peter William**  
**Badhuisweg 3**  
**NL-1031 CM Amsterdam (NL)**  
Inventor: **Vonkeman, Koert Alexander**  
**Badhuisweg 3**  
**NL-1031 CM Amsterdam (NL)**

(54) **Process for the catalytic partial oxidation of hydrocarbon.**

(57) A process for the catalytic partial oxidation of a hydrocarbon feedstock comprises contacting a feed comprising a hydrocarbon feedstock and an oxygen-containing gas at elevated pressure and a temperature of at least 950 °C with a catalyst comprising as a catalytically active metal rhodium, iridium or ruthenium.

**EP 0 629 578 A1**

The present invention relates to a process for the catalytic partial oxidation of hydrocarbons, in particular a process for the preparation of a mixture of carbon monoxide and hydrogen from methane, natural gas, associated gas or other sources of light hydrocarbons.

The partial oxidation of hydrocarbons, for example methane or natural gas, in the presence of a catalyst is an attractive route for the preparation of mixtures of carbon monoxide and hydrogen, which mixtures are known in the art as synthesis gas. The synthesis gas so-produced may be converted into valuable products, for example hydrocarbon fuels boiling in the middle distillate range, prepared by means of the Fischer-Tropsch synthesis, hydrocarbon waxes, lubricating base oils or methanol.

The optimum catalytic partial oxidation process would give high yields of carbon monoxide and hydrogen at elevated pressures, for example about 30 bar, and very high space velocities, for example of the order of 1,000,000 NI/h. For thermodynamic reasons, in order to obtain high yields of carbon monoxide and hydrogen under these process conditions, it is necessary to operate the partial oxidation process at high temperatures. However, at the high temperatures required in such operation, there exists a major problem in maintaining a high level of catalyst activity and selectivity over the prolonged operation times demanded by a commercial process.

The literature contains a number of documents disclosing details of experiments conducted into the catalytic partial oxidation of hydrocarbons, in particular methane, employing a wide range of catalysts. The majority of these experiments, however, have been conducted under very mild conditions or under conditions wholly unsuited to the operation of a commercial catalytic partial oxidation process.

Thus, European Patent Application publication No. 0 303 438 (EP-A-0 303 438) discloses a process for the catalytic partial oxidation of a hydrocarbonaceous feedstock in which a gaseous mixture of the hydrocarbonaceous feedstock, oxygen or an oxygen-containing gas and, optionally, steam, is introduced into a catalytic partial oxidation zone to contact a catalyst retained therein. The catalyst employed in the process may comprise a wide range of catalytically active components, for example palladium, platinum, rhodium, iridium, osmium, ruthenium, nickel, chromium, cobalt, cerium, lanthanum and mixtures thereof. Further, it is stated in EP-A-0 303 438 that materials not normally considered to be catalytically active may also be employed as catalysts, for example refractory oxides such as cordierite, mullite, mullite aluminium titanate, zirconia spinels and alumina. The catalyst may be of a variety of forms, for example sheets of corrugated metal packed to form elongate channels therethrough or wire mesh. However, preference is given in EP-A-0 303 438 to the use of catalysts in the form of monoliths.

European Patent No. 0 262 947 (EP-B-0 262 947) discloses a process for generating hydrogen by the partial oxidation of a hydrocarbon in which a mixture of the hydrocarbon and oxygen is injected into a mass of a catalyst. The catalyst disclosed in EP-B-0 262 947 comprises platinum and chromium oxide supported on a refractory solid.

D.A. Hickman and L.D. Schmidt ("Synthesis Gas Formation by Direct Oxidation of Methane over Pt Monoliths", *Journal of Catalysis* 138, 1992, pages 267 to 282) have conducted experiments into the partial oxidation of methane in the presence of catalysts comprising either platinum or rhodium. The catalysts employed were in the form of a polycrystalline platinum foil or rhodium or platinum supported on a ceramic foam carrier. The partial oxidation reactions were conducted at substantially atmospheric pressure and at temperatures in the range of from 600 to 1500 K (337 to 1237 °C).

A.T. Ashcroft et al. ("Selective oxidation of methane to synthesis gas using transition metal catalysts", *Nature*, vol. 344, No. 6264, pages 319 to 321, 22nd March, 1990) disclose the partial oxidation of methane to synthesis gas in the presence of a range of ruthenium-containing catalysts. The objective of the experiments was to establish that the partial oxidation process could be carried out mild conditions and at low temperatures. To this end, the experiments were conducted with a low gas hourly space velocity of 40,000 /hr, a pressure of 1 atmosphere and a temperature of about 775 °C. A single experiment is reported in which elevated pressures were applied. However, in this case, a large excess of methane was used in order to avoid the risk of explosions.

P.D.F. Vernon et al. ("Partial Oxidation of methane to Synthesis Gas", *Catalysis Letters* 6 (1990) 181-186) disclose a range of experiments in which catalysts comprising nickel, ruthenium, rhodium, palladium, iridium or platinum, either supported on alumina or present in mixed oxide precursors, were applied. Again, the experiments reported are limited to a catalytic partial oxidation process employing only mild operating conditions. As a basis, a set of mild reaction conditions were selected: a pressure of 1 atmosphere, a gas hourly space velocity of 40,000 /hr, a temperature of 1050 K (777 °C) and a methane/oxygen ratio of 2.0. From this basis, each of the process parameters was explored. From this study it was concluded that the low temperature operation gave certain operating advantages, but was only practicable at pressures of the order of 1 atmosphere. The authors report the same experiments in "Partial Oxidation of Methane to Synthesis Gas, and Carbon Dioxide as an Oxidising Agent for Methane Conversion", *Catalysis Today*, 13

(1992) 417-426.

R.H. Jones et al. ("Catalytic Conversion of Methane to Synthesis Gas over Europium Iridate,  $\text{Eu}_2\text{Ir}_2\text{O}_7$ ", Catalysis Letters 8 (1991) 169-174) report the selective partial oxidation of methane using the europium iridium pyrochlore  $\text{Eu}_2\text{Ir}_2\text{O}_7$ . The reaction was studied under the mild conditions of a pressure of 1 atmosphere and a temperature of 873 K (600 °C).

J.K. Hockmuth ("Catalytic Partial Oxidation of Methane over a monolith Supported Catalyst", Applied Catalysis B: Environmental, 1 (1992) 89-100) reports the catalytic partial oxidation of methane using a catalyst comprising a combination of platinum and palladium supported on a cordierite monolith body.

United States Patent No. 5,149,464 (US-A-5,149,464) is directed to a method for selectively oxygenating methane to carbon monoxide and hydrogen by bringing the reactant gas mixture at a temperature of about 650 °C to 900 °C into contact with a solid catalyst which is generally described as being either:

a) a catalyst of the formula  $\text{M}_x\text{M}'_y\text{O}_z$ , where:

M is at least one element selected from Mg, B, Al, Ln, Ga, Si, Ti, Zr and Hf; Ln is at least one member of lanthanum and the lanthanide series of elements;

M' is a d-block transition metal,

and each of the ratios  $x/y$  and  $y/z$  and  $(x+y)/z$  is independently from 0.1 to 8; or

b) an oxide of a d-block transition metal; or

c) a d-block transition metal on a refractory support; or

d) a catalyst formed by heating a) or b) under the conditions of the reaction or under non-oxidising conditions.

The d-block transition metals are said in US-A-5,149,464 to be selected from those having atomic number 21 to 29, 40 to 47 and 72 to 79, the metals scandium, titanium, vanadium, chromium, manganese, iron, cobalt, nickel, copper, zirconium, niobium, molybdenum, technetium, ruthenium, rhodium, palladium, silver, hafnium, tantalum, tungsten, rhenium, osmium, iridium, platinum and gold. It is stated in US-A-5,149,464 that the preferred metals are those in Group VIII of the Periodic Table of the Elements, that is iron, osmium, cobalt, rhenium, iridium, palladium, platinum, nickel and ruthenium.

The process described in US-A-5,149,464 is operated at a temperature in the range of from 650 °C to 900 °C, with a range of from 700 °C to 800 °C being preferred. A range of experiments are described in US-A-5,149,464 in which a variety of catalysts comprising Group VIII metals were tested, including ruthenium oxide, praseodymium/ruthenium oxides, pyrochlores, ruthenium on alumina, rhodium on alumina, palladium on alumina, platinum on alumina, nickel/aluminium oxide, perovskites and nickel oxide.

A similar general disclosure of a catalyst for use in the catalytic partial oxidation process is made in International Patent Application publication No. WO 92/11199. WO 92/11199 specifically discloses experiments in which catalysts comprising iridium, palladium, ruthenium, rhodium, nickel and platinum supported on alumina were applied. All the experiments were conducted under mild process conditions, with typical conditions being a pressure of 1 atmosphere, a temperature of 1050 K (777 °C) and a gas hourly space velocity of about 20,000 /hr. In the text of WO 92/11199 it is stated that extended life tests of the catalysts were underway, but that most catalysts should be expected to show no deterioration in activity after 80 hours, and possible much longer.

As mentioned hereinbefore, to be commercially attractive, a catalytic partial oxidation process should operate at elevated pressures, requiring operating temperatures above those described in the abovementioned documents. A most important factor when considering a catalyst for application in a commercial process, is the stability of that catalyst under the prevailing process conditions. The mild conditions under which the experiments reported in the prior art have been conducted do not provide an insight into the stability of the various catalyst compositions under the severe process conditions needed for commercial implementation. At these severe operating conditions, it has surprisingly been found that a marked difference in the stability of the Group VIII metal catalysts disclosed in the prior art exists. Most surprisingly, contrary to the teaching of WO 92/11199, it has been found that, under commercially applicable conditions, catalysts comprising rhodium, iridium or ruthenium display a significantly higher stability in terms of both selectivity and activity than the remaining Group VIII metal catalysts.

Accordingly, the present invention provides a process for the catalytic partial oxidation of a hydrocarbon feedstock, which process comprises contacting a feed comprising the hydrocarbon feedstock and an oxygen-containing gas at elevated pressure and a temperature of at least 950 °C with a catalyst comprising as a catalytically active metal rhodium, iridium or ruthenium.

The process of the present invention may be used to prepare a mixture of carbon monoxide and hydrogen from any gaseous or hydrocarbon feedstock having a low boiling point. The process is particularly suitable for the partial oxidation of methane, natural gas, associated gas or other sources of light hydrocarbons.

The hydrocarbon feedstock is reacted with an oxygen-containing gas. Air is suitable for use as the oxygen-containing gas. However, the use of substantially pure oxygen as the oxygen-containing gas may be preferred. In this way, the need for handling a large volume of inert gas, for example nitrogen when using air as the oxygen-containing gas, is avoided. The feed may optionally comprise steam.

5 The feed may comprise the hydrocarbon feedstock and the oxygen-containing gas in an amount to give a suitable oxygen-to-carbon ratio. Preferably, the oxygen-to-carbon ratio is in the range of from 0.3 to 0.8, more preferably from 0.45 to 0.75. References to the oxygen-to-carbon ratio refer to the ratio of oxygen in the form of molecules ( $O_2$ ) to carbon atoms present in the hydrocarbon feedstock. Preferably, the oxygen-to-carbon ratio is in the range of from 0.45 to 0.65, with oxygen-to-carbon ratios of about the stoichiometric ratio, 0.5, being especially preferred. If steam is present in the feed, the steam-to-carbon ratio is preferably in the range of from above 0.0 to 3.0, more preferably from 0.0 to 2.0. The hydrocarbon feedstock, the oxygen-containing gas and the steam, if present, are preferably well mixed prior to being contacted with the catalyst.

15 The process of the present invention is operated at elevated pressures, that is pressures significantly above atmospheric pressure. The process may be operated at pressures in the range of up to 150 bar. Preferably, the operating pressure is in the range of from 3 to 100 bar, more preferably from 10 to 75 bar.

Under the conditions of high pressure prevailing in the process, it is necessary to allow the feed to contact the catalyst at elevated temperatures in order to achieve the desired high level of conversion. Accordingly, the process is operated at temperatures of at least  $950^\circ\text{C}$ . Preferably, the operating temperature is in the range of from  $950$  to  $1300^\circ\text{C}$ , more preferably from  $950$  to  $1200^\circ\text{C}$ . Advantageously, 20 the feed is preheated prior to being contacted with the catalyst.

The feed may be provided during the process at any suitable space velocity, with high gas hourly space velocities being preferred. Thus, typical space velocities for the process are in the range of from about 20,000 to about 50,000  $\text{NI/hr}$ , more preferably in the range of from about 50,000 to about 20,000,000  $\text{NI/hr}$ . Space velocities in the range of from 500,000 to 10,000,000  $\text{NI/hr}$  are particularly 25 suitable.

The catalyst employed in the process of the present invention comprises as a catalytically active component a metal selected from rhodium, iridium or ruthenium. Catalysts comprising rhodium are particularly preferred.

30 The catalytically active metal is most suitably supported on a carrier. Suitable carrier materials are well known in the art and include the refractory oxides such as silica, alumina, titania, zirconia and mixtures thereof. The catalytically active metal may be deposited on the refractory oxide carrier by techniques well known in the art. A most suitable method for depositing the metal on the carrier is impregnation, which method typically comprises contacting the carrier material with a solution of a compound of the catalytically 35 active metal, followed by drying and calcining the resulting material.

Any suitable reaction regime may be employed for the process of the present invention to contact the feed with the catalyst. One suitable reaction regime is a fluidised bed, in which the catalyst is employed in the form of particles. A preferred reaction regime for use in the process is a fixed bed reaction regime, in which the catalyst is retained in the reaction in a fixed arrangement. In the fixed bed regime, the catalyst 40 may again be in the form of particles. Alternatively, the catalyst may have the form of a foam, prepared, for example, by the impregnation of a ceramic foam by the method discussed hereinabove. Suitable ceramic foams for use in the preparation of the catalyst include those having from 30 to 150 pores per inch (12 to 60 pores per centimetre). Further alternative forms for the catalyst include refractory oxide, honeycomb monolith structures and metal gauzes, with the catalytically active metal being deposited on the honeycomb 45 monolith or gauze.

In a preferred embodiment of the process of this invention, the feed is contacted with a catalyst retained in a fixed bed arrangement, which arrangement has a high tortuosity. The term "tortuosity" is a common term in the art which, when referring to a fixed catalyst bed, can be defined as the ratio of the length of the path taken by a gas flowing through the bed to the length of the shortest straight line path 50 through the bed. Thus, the honeycomb monolith structures have a tortuosity of 1.0. For the purposes of the present invention, the term "high tortuosity" is a reference to arrangements having a tortuosity substantially greater than that of the honeycomb monolith structures, in particular a tortuosity of at least 1.1. A fixed bed of catalyst particles typically has a tortuosity of about 1.5, whilst ceramic foams may be prepared having a tortuosity in the range of from 3.0 to 4.0, or even higher. In general, the tortuosity of the fixed bed 55 arrangement is preferably in the range of from 1.1 to about 10.0, more preferably to about 5.0. A most suitable range of tortuosity is from 1.3 to 4.0.

It has been found that by employing the catalyst in a fixed bed arrangement having a high tortuosity allows the required conversion to be achieved with only a relatively very short contact time between the

reacting gases and the catalyst. In this way, only a very low volume of catalyst is required, which in turn allows the very high gas space velocities desirable for operating a commercial process to be achieved.

The feed is preferably contacted with the catalyst under adiabatic conditions. For the purposes of this specification, the term "adiabatic" is a reference to reaction conditions in which substantially all heat loss and radiation from the reaction zone is prevented, with the exception of heat leaving in the gaseous effluent stream of the reactor.

In a further aspect, the present invention relates to carbon monoxide or hydrogen whenever prepared by a process as hereinbefore described.

The mixture of carbon monoxide and hydrogen prepared by the process of this invention is particularly suitable for use in the synthesis of hydrocarbons, for example by means of the Fischer-Tropsch synthesis, or the synthesis of oxygenates, for example methanol. Processes for the conversion of the mixture of carbon monoxide and hydrogen into such products are well known in the art.

The process of the present invention is further described by way of the following illustrative examples, in which Examples 1 to 3 each exemplify a process according to the present invention and Examples 4 and 5 are for comparative purposes.

### Example 1

#### Catalyst Preparation

12.93 g of an aqueous solution, prepared by dissolving sufficient rhodium trichloride ( $\text{RhCl}_3$ ) in water to give a rhodium concentration of 4.12 % by weight, was concentrated by evaporation to a volume of 3.5 ml. Alpha alumina extrudates (1.0 mm diameter trilobes, commercially available ex. Dycat, 10g) were impregnated by immersion in the aforementioned solution. The resulting extrudates were dried in an oven at a temperature of  $120^\circ\text{C}$  and subsequently calcined at a temperature of  $500^\circ\text{C}$ . The resulting catalyst comprised 5.0 % by weight rhodium.

#### Catalytic Partial Oxidation

A reactor was constructed comprising a transparent sapphire tube. The rhodium-containing catalyst prepared as hereinbefore described was crushed and loaded into the sapphire tube and retained in the form of a fixed bed of catalyst particles having a tortuosity of about 1.5. Methane and oxygen, in sufficient amounts to give an oxygen-to-carbon ratio of 0.52, were thoroughly mixed just before being introduced into the reactor to contact the fixed bed of catalyst. The mixture of methane and oxygen was fed to the reactor at a pressure of 4.5 bar and at a gas hourly space velocity (GHSV) of 2,000,000  $\text{NI}/\text{hr}$ .

The operating temperature of the catalyst bed was measured by optical pyrometry. The composition of the gas mixture leaving the reactor was determined by gas chromatography and weighing water condensed from the gas stream leaving the reactor. The conversion of methane and the selectivity of the process to carbon monoxide and hydrogen (on the basis of methane converted) was determined. The operating conditions of the reactor and the results of the experiment are summarised in the Table hereinbelow.

### Example 2

Using the same general procedure as described in Example 1, a ruthenium-containing catalyst was prepared by impregnation of the alpha-alumina extrudates using an aqueous solution of hexamine ruthenium (III) chloride ( $\text{Ru}(\text{NH}_3)_6\text{Cl}_3$ ). The resulting catalyst comprised 5.0 % by weight ruthenium.

The thus prepared catalyst was loaded into the apparatus and tested for activity in the catalytic partial oxidation of methane using the same general procedure as described in Example 1. The operating conditions of the reactor and the results of the experiment are summarised in the Table hereinbelow.

### Example 3

Using the same general procedure as described in Example 1, an iridium-containing catalyst was prepared by impregnation of the alpha-alumina extrudates using an aqueous solution of chloroiridic acid ( $\text{H}_2\text{IrCl}_6$ ). The resulting catalyst comprised 5.0 % by weight iridium.

The thus prepared catalyst was loaded into the apparatus and tested for activity in the catalytic partial oxidation of methane using the same general procedure as described in Example 1. The operating conditions of the reactor and the results of the experiment are summarised in the Table hereinbelow.

Example 4 Comparative Example

Using the same general procedure as described in Example 1, a platinum-containing catalyst was prepared by impregnation of the alpha-alumina extrudates using an aqueous solution of chloroplatinic acid ( $\text{H}_2\text{PtCl}_6$ ). The resulting catalyst comprised 5.0 % by weight platinum.

The thus prepared catalyst was loaded into the apparatus and tested for activity in the catalytic partial oxidation of methane using the same general procedure as described in Example 1. The operating conditions of the reactor and the results of the experiment are summarised in the Table hereinbelow.

Example 5 Comparative Example

Using the same general procedure as described in Example 1, a palladium-containing catalyst was prepared by impregnation of the alpha-alumina extrudates using an aqueous solution of tetraaminepalladium(II) nitrate ( $\text{Pd}(\text{NH}_3)_4(\text{NO}_3)_2$ ). The resulting catalyst comprised 5.0 % by weight palladium.

The thus prepared catalyst was loaded into the apparatus and tested for activity in the catalytic partial oxidation of methane using the same general procedure as described in Example 1. The operating conditions of the reactor and the results of the experiment are summarised in the Table hereinbelow.

From the data presented in the Table, it can be seen that, under the conditions of elevated temperature and pressure applied, catalysts comprising rhodium, ruthenium or iridium exhibited very high levels of stability in terms of both the overall conversion of methane and the selectivity to hydrogen and carbon monoxide. None of the catalysts comprising rhodium, ruthenium or iridium exhibited significant losses in activity or selectivity, with the high levels of performance being maintained over the entire runtime of the experiments.

The catalytic partial oxidation reactions were performed using the rhodium-containing catalyst in a further prolonged experiment for a total runtime of 160 hours under the conditions of Example 1, as set out in the Table. No perceptible loss in activity or selectivity of the catalyst was observed.

In contrast, it can be seen that the catalysts comprising platinum and palladium exhibited much poorer levels of stability under the prevailing process conditions, with significant rates of deactivation in both the overall process conversion and selectivity being experienced. The experiments employing both the platinum- and palladium-containing catalysts had to be stopped after the very short runtimes indicated in the Table owing to the formation of coke on the catalyst, leading to a marked increase in the pressure drop across the catalyst bed and a significant rise in the catalyst operating temperature.

Table

Example No.	1	2	3	4	5
Active metal	rhodium	ruthenium	iridium	platinum	palladium
Operating Conditions					
Temperature ( $^{\circ}\text{C}$ )	968	1000	980	1060	1220
Pressure (bar)	4.5	3.9	4.0	3.8	3.9
GHSV (1000 $\text{NI}/\text{hr}$ )	2000	2000	2000	2000	2000
oxygen/carbon ratio	0.52	0.52	0.52	0.52	0.52
runtime (hours)	24	24	24	2	2
$\text{CH}_4$ conversion (%)	81.9	73.7	77.1	66.0	60.8
$\text{CO}$ selectivity (%) <sup>1</sup>	91.8	80.0	84.4	70.0	69.4
$\text{H}_2$ selectivity (%) <sup>2</sup>	90.3	88.4	89.7	83.2	76.4
Deactivation (%) <sup>3</sup>					
$\text{CH}_4$ conversion	<0.1	<0.1	<0.1	1.7	2.5
$\text{H}_2$ selectivity	<0.1	<0.1	<0.1	1.4	2.6

1 selectivity to  $\text{CO}$  based on  $\text{CH}_4$  conversion

2 selectivity to  $\text{H}_2$  based on  $\text{CH}_4$  conversion

3 deactivation in terms of % performance lost per hour of runtime

## Claims

1. A process for the catalytic partial oxidation of a hydrocarbon feedstock, which process comprises contacting a feed comprising a hydrocarbon feedstock and an oxygen-containing gas at elevated pressure and a temperature of at least 950 °C with a catalyst comprising as a catalytically active metal rhodium, iridium or ruthenium.
2. A process according to claim 1, characterised in that the hydrocarbon feedstock comprises methane, natural gas, associated gas or a source of light hydrocarbons.
3. A process according to either of claims 1 or 2, characterised in that the oxygen-containing gas is substantially pure oxygen.
4. A process according to any preceding claim, characterised in that the feed comprises the hydrocarbon feedstock and the oxygen-containing gas in amounts giving an oxygen-to-carbon ratio of from 0.3 to 0.8, preferably from 0.45 to 0.75, more preferably from 0.45 to 0.65.
5. A process according to any preceding claim, characterised in that the feed is contacted with the catalyst at a pressure in the range of up to 150 bar, preferably from 3 to 100 bar, more preferably from 10 to 75 bar.
6. A process according to any preceding claim, characterised in that the feed is contacted with the catalyst at a temperature in the range of from 950 to 1300 °C, preferably from 950 to 1200 °C.
7. A process according to any preceding claim, characterised in that the feed is contacted with the catalyst at a gas hourly space velocity in the range of from 20,000 to 50,000,000 NI/l/hr, preferably from 50,000 to 20,000,000 NI/l/hr, more preferably from 500,000 to 10,000,000 NI/l/hr.
8. A process according to any preceding claim, characterised in that the catalyst comprises rhodium.
9. A process according to any preceding claim, characterised in that the catalyst is retained in a fixed bed arrangement, preferably a fixed bed arrangement having a high tortuosity, more preferably having a tortuosity in the range of from 1.1 to 5.0.
10. A process according to claim 9, characterised in the catalyst is in the form of a ceramic foam impregnated with the catalytically active metal.
11. A process according to any preceding claim, characterised in that the feed is contacted with the catalyst under substantially adiabatic conditions.
12. Carbon monoxide or hydrogen whenever prepared by a process according to any of claims 1 to 11.



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# EUROPEAN SEARCH REPORT

Application Number  
EP 94 20 1732

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.5)
X	EP-A-0 537 862 (SHELL INTERNATIONALE RESEARCH MAATSCHAPPIJ B.V.) * claims 1,5,10-13; example 1 *	1-8	C01B3/40
A	US-A-4 087 259 (YOSHIYASU FUJITANI ET AL) * claim 1 *	1	
A,D	WO-A-92 11199 (ISIS INNOVATION LTD) * claim 1 *	1	
			TECHNICAL FIELDS SEARCHED (Int.Cl.5)
			C01B
The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 10 October 1994	Examiner Clement, J-P
CATEGORY OF CITED DOCUMENTS			
<p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons A : member of the same patent family, corresponding document</p>			